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(54) Title: LEAD-FREE SOLDER ALLOY POWDER PASTE USE IN PCB PRODUCTION

(57) Abstract

Tombitoning susceptibility and reflow peak temperature reduction of solder alloys, in particularly lead-free solder alloys, has been found to be schieved effectively by mixing the solder alloy in the form of an alloy passe with a low melting alloy utilized in powder form, in particular 82—toroitating alloy.

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## LEAD-FREE SOLDER ALLOY POWDER PASTE USE IN PCB PRODUCTION

This invention relates to lead-free solder alloy powder usage in pastes for soldering components to printed circuit boards (PCB's).

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When lead-free solders are used in the soldering of components to printed circuit boards, problems stem from the increase in reflow (soldering) temperature required by the main lead-free alternatives relative to the eutectic Sn(PbAg) solders currently used. The principal lead-free solders are based on the tin-copper, tin-silver and tin-silver-copper eutectics, melting at 227°C, 221°C and 217°C, respectively. These alloys require relatively high reflow temperatures in the range 230-240°C to obtain adequate soldering. Reflow temperatures in this range may damage temperature sensitive components. Thus, lead free solders have not yet found widespread adoption in electronics assembly despite their obvious advantages.

In order to lower lead-free alloy melting points below 217°C, it is possible to alloy the above mentioned lead-free solders with limited amounts of bismuth, generally up to about 10%, typically 2-5% by weight. There is indeed an additional advantage in using bismuth in solid solution in tin in lead-free alloys in that the bismuth has been found to strengthen the lead-free alloys. The addition of bismuth has, however, the disadvantage of introducing a melting range. Thermal strains developing in an assembly on cooling, in conjunction with solder joints with a freezing range can, in unfavourable circumstances, lead to hot cracking. This phenomenon of hot cracking has been observed particularly in plated-through-hole

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applications but not in surface mount reflow soldering, so bismuth containing alloys are viable in many solder paste applications.

A defect commonly found on reflow soldered printed circuit boards is that when chip components solder faster at one end than another and as a consequence are pulled by surface tension, they stand vertically on one pad, creating an electrical discontinuity. It is for this reason that this behaviour is known as tombstoning. In current practice this is addressed by using a solder alloy with a melting range, but, where lead-free solders are concerned, no solution has been proposed.

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Sn-Ag-Bi and Sn-Ag-Cu-Bi alloy compositions are well documented as lead-free solder alloys. The concept of combining high and low melting point alloy powders to form a mixture which melts at a low temperature but forms a high melting point joint is also well documented. However, the use of such alloys with a melting range to inhibit tombstoning is not known, and has not been documented.

25 We have found that solder pastes made with mixtures of Sn63Pb37 powder and Sn62Pb16Ag2 powder, melting at 183°C and 179°C respectively surprisingly give a significantly reduced tendency to tombstoning as compared to pastes made up with prealloyed powders,

30 when used to solder chip components on printed circuit boards.

On this basis we have concluded that use of a mixture of a SnB1 alloy powder, such as a SnA3Bi57 powder, and a SnAgCu alloy powder, such as Sn96.5Ag1.8Cu0.7 powder, such specific alloys melting

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at 138°C and 217°C respectively, in a (lead-free) paste, will analogously also have an anti-tombatoning effect as well as enable the paste to start to reflow at a lower temperature than if prealloyed powder were used.

According to one aspect of the present invention, there is provided a method of securing a chip component to a printed circuit board and, in so doing, achieving the combined effects of reducing tombetoning and reducing solder paste reflow temperature, which comprises carrying out soldering with a paste of a first solder alloy powder to which is added a powdered lower melting alloy which melts at a lower temperature than said first solder alloy and which, when admixed with the paste of the first solder alloy, forms a higher melting point joint than that attainable with only the paste of the second solder alloy.

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In a second aspect, this invention provides a method of reducing susceptibility to tombetoning and reducing the melting point of a lead-free solder alloy in a solder paste being used to attach this component to a printed circuit board, which comprises adding to a paste of a first solder alloy powder, which paste is a lead-free solder paste, a SmBi alloy powder, which is lower melting than the first solder alloy powder, to produce a bismuth containing final alloy containing from 1-10% bismuth, the first solder alloy containing 0-5% Ct., 0-10% Ag and 0-5% St., the remainder being Sn and at least one of Cu, Ag and Sb being present in a minimum anounce of Cu.

All percentages expressed herein are on a weight basis.

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Addition of SnBi powder addition to a lead-free solder paste, in particular SnBgCu solder paste is particularly noteworthy in that the paste starts to reflow at a lower temperature, reducing the required peak reflow temperature.

We have further found that the reduction in tombstoning is enhanced if the lower melting alloy is present as a finer size powder than the higher melting alloy which is present as a larger size powder. Preferably, the lower melting point alloy is employed in the form of a powder of which the particle size is predominantly less than 25  $\mu m$  diameter, while the first solder alloy powder particle size is predominantly greater than 25  $\mu m$  diameter. More preferably, the lower melting point allow particle size is predominantly in the range 10-25 um and the first solder allow particle size is predominantly 20-45 mm. By the word predominately, it is meant that more than 50% by wt., preferably more than 75% and most preferably all of the alloy in question has the indicated particle size. It is hypothesised that the fine lower melting powder particles melt first and form a network of liquid around the larger powder particles. This liquid network enables wetting to take place more readily and initiate reflow, and maximises the effective melting range to minimise tombstoning.

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In preferred practice, there is used a starting alloy containing up to 3% Cu, up to 5% Ag, and up to 5% Sb, the remainder being Sn and at least one of the elements Cu, Ag and Sb being present in an amount of at least 0.1%

It is found typically in the practice of this invention that, when using a starting alloy of SnAg3.8,

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Cu0.7 in the form of a solder paste to which Sn43Bi57 is added in powder form in an amount to give an alloy having an overall content of 5% Bi, as a result of the SnBi allow powder addition, the reflow temperature needed is reduced by about 10°C. This is noticeably greater than the 2°C reduction in liquidus temperature expected with 5% Bi addition to a SnAqCu eutectic. It is considered that this enhanced behaviour results from adding the bismuth as a powder concentrate to the other components already in alloy form, instead of using a homogeneous alloy, in that latent heat of melting is absorbed over a greater temperature range, starting at 138°C, the melting point of the SnBi eutectic, thereby reducing temperature lag between PCB and solder joint and allowing a lower reflow peak temperature than is achieved when using the equivalent homogeneous alloy, paste containing Bi.

A further advantage of the use of SnBi as powder admixture stems from the fact that, in solder pastes, the oxide content of the powder needs to be as low as possible, to give good reflow. Adding bismuth to a high tin or tin-lead solder in conventional manner changes the oxide formed on the powder surface from tin oxide to mixed oxide containing bismuth as well as tin. The mixed oxide grows faster that the tin oxide, so bismuth alloy solder powders contain more oxide than non-bismuth alloy solders, and deteriorate faster in storage. Making the alloy using a powder and mixture will give a lower overall oxide content, hence better storage and reflow properties.

It has already been stated herein that the final alloy should have a Bi content of 1-10% this amount preferably being in the range from 2-0% and most preferably being about 5%. To to 1% of Ar. Cu and Sb

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can each be employed in the bismuth containing additive alloy which preferably contains 40-70% Bi and the remainder tin. Because of these two factors, if one or more of Ag, Cu and Sb is to be present, preferably care should be taken to have the final alloy show the following analysis:

Ag up to 6%
Cu up to 3%
10 Sb up to 5%
Bi 1-10%
Sn rest

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#### CLAIMS

1. A method of securing a chip component to a printed circuit board and, in so doing, achieving the combined effects of reducing tombstoning and reducing solder paste reflow temperature, which comprises carrying out soldering with a paste of a first solder alloy powder to which is added a powdered lower melting alloy which melts at a 10 lower temperature than said first solder allow and which, when admixed with the paste of the first solder alloy, forms a higher melting point joint than that attainable with only the paste of the

second solder alloy. 15

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and reducing the melting point of a lead-free solder alloy in a solder paste being used to attach chip component to a printed circuit board. 20 which comprises adding to a paste of a first solder allow powder, which paste is a lead-free solder paste, a SnBi alloy powder, which is lower melting than the first solder alloy powder, to produce a bismuth containing final alloy 25 containing from 1-10% bismuth, the first solder alloy containing 0-5% Cu, 0-10% Ag and 0-5% Sb, the remainder being Sn and at least one of Cu, Aq

A method of reducing susceptibility to tombstoning

and Sb being present in a minimum amount of 0.1%.

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30 з. A method as claimed in Claim 2, wherein the first solder alloy powder contains from 0.1-3% Cu, from 0.1-5% Ag and from 0.1-5% Sb.

4. A method as claimed in Claim 2, wherein the first solder alloy powder has the composition SnAg3.8Cu0.7.

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A method as claimed in any preceding claim. wherein the final alloy has a Bi content in the range from 2-6%.

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A method as claimed in any one of Claims 2 to 3. 6. wherein the SnBi alloy powder contains from 40-70% Ri.

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A method as claimed in Claim 7, wherein the SnBi alloy powder additionally contains one of more of Aq, Cu and Sb.

A method as claimed in any one of Claims 2-8, wherein the final alloy has an analysis:-

rest

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Ag up to 6% Cni up to 3% Sh up to 5% Вi 1-10%

Sn

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A method as claimed in any preceding claim which is applied to the production of a solder pad affixing a component to the surface of a conductor on a dielectric substrate.

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10. A method as claimed on any one of claims 1-9. wherein the lower melting point alloy is employed in the form of a powder of which the particle size is predominately less than 25 µm diameter, while the first solder allow powder particle size is predominately greater than 25 um diameter.